Gieras, J.F. and Wing, M.: *Permanent Magnet Motors Technology: Design and Applications*. Marcel Dekker, New York, 2nd edition, 2002.

ERRATUM

Page, line, eqn, Fig. or Table	**Errors found by authors**	**Should be replaced with…**
p. 7, 1st line from top	Fig.1.4	Fig. 1.4a
p. 12, Table 1.2, 3rd row, 3rd column	403.3	433.3
p. 27, Fig. 1.26, caption	hydraulic	hydro
p. 30, below eqn. (1.5)	$n_2/n_2 = \|N_1/N_2\|$	$n_2/n_2 = \|z_1/z_2\|$
p.32, 6th line from top	Ns/m	Nms/rad
p.32, 7th line from top	N/m	Nm/rad
p.37, 6th line from bottom	$T_{rms}^2(t_1+t_2+t_3+...T_n) =$	$T_{rms}^2(t_1+t_2+t_3+...t_n) =$
p. 37, 5th line from bottom	$T_{rms}^2 = \sum t_i = \sum T_i^2 t_i$	$T_{rms}^2 \sum t_i = \sum T_i^2 t_i$
p. 39, 12th line from top	...at T_r = 60 Nm...	...at resisting torque T_r = 60 Nm...
p. 40, 16th line from bottom	"…stator core wound from electrotechnical steel strip."	"…stator core.'
p. 53, 8th line from top	... of B_r is 0.03 to 0.045%/^{0}C.	... of B_r is -0.03 to -0.045%/^{0}C.
p. 53, 9th line from top	... of H_c is 0.14 to 0.40%/^{0}C.	... of H_c is -0.14 to -0.40%/^{0}C.
p. 60, below eqn (2.25)		The following explanation is necessary: $F_c = H_c H_M$; $\Phi_r = B_r S_M = B_r w_M h_M$
p. 79, 7th line from bottom	$= \frac{1}{0.4\pi\times10^{-6}}\frac{1.25-0}{650{,}000-0} \approx$	$= \frac{1}{0.4\pi\times10^{-6}}\frac{1.25-0}{950{,}000-0} \approx$
p. 79, 5th line from bottom	$B_g =$	$B_g \approx$
p. 79, 4th line from bottom	...according to eqn (2.24)	...according to eqn (2.24) in which $B = B_g$ and $H = H_g$ is
p. 80, 7th line from bottom	$B_g =$	$B_g \approx$
p. 134, below eqn (4.33)	where $k_C \geq 1$ is the Carter's coefficient and $k_{sat} \geq 1$ is saturation factor of the magnetic circuit according to eqn (2.48). For most PM machines the air gap $g' = k_C k_{sat} g + h_M/\mu_{rrec}$ where g is the mechanical clearance.	For most PM machines the air gap $g' = k_C k_{sat} g + h_M/\mu_{rrec}$ where g is the mechanical clearance, $k_C \geq 1$ is Carter's coefficient and $k_{sat} \geq 1$ is the saturation factor of the magnetic circuit according to eqn (2.48).
p. 175, 9th line from top	...winding is slower...	...winding or in PM conductive material is slower...
p. 189, Table 5.2 caption	Table 5.2. Reaction factors for PM synchronous machines	Table 5.2. Form factors of the armature reaction for PM synchronous machines
p. 205, eqn (5.93) and p. 206, eqn (5.98)	$\cos(\nu p\alpha \pm \omega_\nu t)$ (ν is the number of higher harmonics)	It would be better to write $\cos(\nu p\alpha \pm \omega_n t)$ (ν is the number of higher space harmonics and n is the number of higher time harmonics, i.e. generated by inverter)

p. 205, eqn (5.94) and p. 206, eqn (5.99)	$\cos(\nu p\alpha \pm \omega_{\mu}t + \phi_{\nu})$	It would be better to write $\cos(\mu p\alpha \pm \omega_{\mu,n}t + \phi_{\mu,n})$ ($\omega_{\mu,n}$ is the angular frequency of the μ^{th} space harmonic of the rotor field for he given n^{th} time harmonic)
p. 207, eqn (5.103)	$k_{ok}\cos(k z_1 \alpha)$	$k_{ok}^2\cos(k z_1 \alpha)$
p. 208, caption under Fig. 5.12	$p = 5$	$p = 3$
p. 208, eqn (5.111), last term	$\sum_{l=1}^{\infty} A_l\cos(l\alpha)$	$\sum_{k=1}^{\infty} A_k\cos(k\alpha)$
p. 210, 8th line from bottom	...of the stator of the r^{th} order...	...of the stator core of the r^{th} order...
p. 210, 3rd line from bottom	...of the frame h_{cf} and ...	...of the core (yoke) h_{cf} and ...
p. 210, 2nd line from bottom	...to the frame diameter D_{cf}, i.e.,	...to the core average diameter D_{cf}, i.e.,
p.247, 10th line from top	"…Lorzentz…"	"…Lorentz…"
p. 247, 17th line from bottom	The cogging torque is...	Neglecting the armature reaction and magnetic saturation, the cogging torque is...
p. 247, 1st line from bottom	"… of of the air gap…"	"… of the air gap…"
p. 248, below eqn (6.45)	"...to one pole pitch skew..."	"...to one slot pitch skew..."
p. 248, eqn (6.47)	k_{ok}	k_{ok}^2
p. 249, eqn (6.51)	$\zeta_k = k_{ok}k_{skk}$	$\zeta_k = k_{ok}^2 k_{skk}$
p. 251, caption under Fig. 6.12	"…c) $b_{sk}/t_1 = 0.95$…"	Delate "$b_{sk}/t_1 = 0.95$"
p. 252, 9th line from bottom	"... dependent of the..."	"... dependent on the..."
p. 254, eqn. (6.64)	$e_{fA}(t) = -N_1\frac{d}{dt}\left[k_{d\mu}\Phi_f(t)\right]$	$e_{fA}(t) = -N_1\left[k_{d1}\frac{d\Phi_{f1}(t)}{dt} + k_{d3}\frac{d\Phi_{f3}(t)}{dt} + ...\right]$
p. 257, eqns (6.65) and (6.66)		Replace ν with n (time harmonics)
p. 257, 2nd line from bottom	The fundamental frequency of torque ripple due to phase commuation is $f_{com} = 2pm_1f$.	Predominant frequencies of torque ripple due to phase commutation are $f_{com} = 2lm_1f$, where $l = 1,2,3,\ldots$.
p. 283, 15th line from bottom	structurely	structurally
p. 245, 9th line from bottom	...when the the supply voltage...	...when the supply voltage...
p. 516, eqn (12.44)	$p = \sqrt{\frac{1}{T_p}\int_0^{T_p} p(t)dt}$	$p = \sqrt{\frac{1}{T_p}\int_0^{T_p} [p(t)]^2 dt}$
p. 516, 10th line from bottom	emiting	emitting
p. 517, Fig. 12.3	Line for $r = 4$ is invisible	
p. 546, eqn (A.5), 3rd term	$\frac{2h_3}{b_{12} + b_{14}}$	$\frac{2h_{13}}{b_{12} + b_{14}}$

p. 547, eqn (A.12)	$l_{1e} \approx (0.083p + 1.217)\frac{pD_{1in} + h_{1t}}{2p}$ + 0.02	$l_{1e} \approx (0.05p + 1.2)\frac{\pi(D_{1in} + h_{1t})}{2p}\frac{w_c}{\tau}$ + 0.03
p. 558, below *F*		$F_c = H_c h_M$ MMF per pole corresponding to coercivity H_c
p. 560, 9th line from top	S_M cross section area of PM $S_M = w_M L_M$ or $S_M = b_p L_M$	S_M cross section area of PM $S_M = w_M l_M$ or $S_M = b_p l_M$
p. 562, 10th line from top	*c* commutation	*c* coercive; commutation
p. 578, 7th line from bottom	[227] Permanent magnet motor with low cogging torque by simulated magnetic field analysis. Shin-Etsu Chemical Co Ltd, Magnetic...	[227] Shin-Etsu Chemical Co Ltd. Permanent magnet motor with low cogging torque by simulated magnetic field analysis. Magnetic...
p. 588, 1st column, 19th line from tom	Pole pitch, 132, 172, 370, 317	Pole pitch, 132, 172, 317, 370